



# Optimization synthesis of carbon nanotubes-anatase TiO<sub>2</sub> composite photocatalyst by response surface methodology for photocatalytic degradation of gaseous styrene

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## ABSTRACT

In present study, the center composite design in response surface methodology (RSM) was firstly applied to optimize the synthesis of multi-wall carbon nanotubes (MWCNTs)–TiO<sub>2</sub> composite photocatalyst. Twenty-eight composite photocatalysts were prepared by adjusting four operating parameters (amount of MWCNTs, amount of TiF<sub>4</sub>, hydrothermal temperature and hydrothermal time) at five levels by the method of multiple variable analysis. The structural, optical and morphological properties of the prepared composite photocatalysts were characterized by X-ray diffraction, UV–visible absorption spectra and scanning electron microscopy, respectively. Based on the experimental design, a semi-empirical expression was firstly established and subsequently applied to predict the photocatalytic degradation activity of the prepared composite photocatalysts to gaseous styrene in a cubic flow-through reactor. The results showed that the experimental photocatalytic degradation efficiencies using the differently prepared MWCNTs–TiO<sub>2</sub> composite photocatalysts matched with the theoretically predicted values very well with a high correlation ( $R^2 = 0.9790$ ). Based on the theoretical and experimental results, the optimum synthesis parameters for the composite photocatalyst within the experimental ranges were 0.01 g MWCNTs, 0.14 g TiF<sub>4</sub>, and 120 °C hydrothermally treated for 87.2 h. The photocatalytic degradation efficiency of gaseous styrene using the MWCNTs–TiO<sub>2</sub> composite photocatalyst synthesized under the optimum parameters reached 74.4%. All these demonstrates that the experimental design and theoretical prediction methods used in this work would have great significance in designing and developing high performance photocatalysts for environmental remediation and solar energy conversion.

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## 1. Introduction

During the last decade, photocatalytic oxidation has become an attractive technology for volatile organic compounds (VOCs) abatement [1–8]. Its appeal lies in its potential to mineralize various VOCs into less toxic or harmless compounds under mild conditions [9,10]. As known, photocatalyst plays an important role in the photocatalytic oxidation process. Among the abundant developed photocatalysts, TiO<sub>2</sub> has been found as the most potential photocatalyst for photocatalytic reactions due to its superior photocatalytic oxidation ability, nonphotocorrosive, nontoxic, and inexpensive characteristics [11–15]. However, relative low photocatalytic degradation efficiency is often obtained due to both the high rate of electron–hole recombination in TiO<sub>2</sub> particles and small

specific surface area for the limited adsorption of VOCs. Hence, development of high performance TiO<sub>2</sub>-based photocatalysts is still an attractive topic for environmental applications.

Recently, the significant interest has been dedicated to enhance the photocatalytic activity of TiO<sub>2</sub> by doping carbon nanotubes (CNTs) towards photocatalytic degradation of VOCs [16–19]. By using these prepared CNTs–TiO<sub>2</sub> composite as photocatalysts, CNTs can not only act as an electron reservoir to suppress the recombination of photo-generated electron–hole pairs, but also act as an excellent adsorbent for VOCs owing to their hollow and layered structures with large specific surface area, which can subsequently enhance the photocatalytic activity of TiO<sub>2</sub>. For instance, Yu et al. [16] synthesized the CNTs–TiO<sub>2</sub> composites with different content of CNTs by the modified sol–gel method, and found that the composites possessed high photocatalytic activity for degradation of acetone in air. Xu et al. [17] prepared CNTs–TiO<sub>2</sub> composite photocatalysts using a simple impregnation method by changing the additive amount of titanium source, and the prepared

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**Table 1**  
Values and levels of chosen variables for central composite design.

Variable	Symbol	Coded levels				
		−2	Low (−1)	Center (0)	High (+1)	+2
Amount of MWCNTs (g)	A	0.01	0.03	0.05	0.07	0.09
Amount of TiF <sub>4</sub> (g)	B	0.02	0.11	0.20	0.29	0.38
Hydrothermal temperature (°C)	C	120	150	180	210	240
Hydrothermal time (h)	D	12	32	52	72	92

photocatalysts exhibited the enhanced photocatalytic activity for benzene degradation. While Yu et al. [18] embedded different amount of CNTs inside the mesoporous TiO<sub>2</sub> aggregates by a facile one-pot hydrothermal method, and the CNTs–TiO<sub>2</sub> composite displayed higher photocatalytic activity for degrading gaseous acetone than that of pristine TiO<sub>2</sub> counterpart. However, although various CNTs–TiO<sub>2</sub> composites were synthesized using different methods, all these reported works applied the approach of single-variable-at-a-time. Such synthetic approach often varies one of the investigated parameter while keeping others as constants, which is usually unable or time consuming to obtain the optimum conditions for the fabrication of high performance composite photocatalysts due to ignoring the interactions and influence among the synthesized parameters. Therefore, development of an efficient experimental design strategy for fabrication of high performance CNTs–TiO<sub>2</sub> composite photocatalysts is highly desired in the field of environmental remediation.

Response surface methodology (RSM) is one of the experimental design techniques that are commonly used for process analysis and modeling [20–24]. The interactions of possible influencing factors on desired responses can be evaluated with RSM just by using minimum number of designed experiments and then an optimal reaction condition can be much easily accomplished. However, no publications to date have applied the RSM to optimize various affecting preparation factors for the synthesis of CNTs–TiO<sub>2</sub> composite photocatalysts.

In present work, RSM was firstly applied to optimize the synthetic parameters for the hydrothermal preparation of CNTs–TiO<sub>2</sub> composite photocatalysts by changing four controlling factors (amount of CNTs, amount of TiF<sub>4</sub>, hydrothermal temperature and hydrothermal time) at five levels. The desired response values (degradation efficiency of styrene) predicted using RSM were compared with experimental photocatalytic degradation efficiencies of gaseous styrene. In addition, the relationship between the photocatalytic activity of the prepared CNTs–TiO<sub>2</sub> composite photocatalysts for degradation of styrene and the synthesis parameters was also discussed based on the experimental results.

## 2. Experimental

### 2.1. Central composite design for preparation of photocatalysts

The chemometric approach was performed using a central composite design (CCD). Analysis of the experimental data was supported by the Design-Expert software (trial version 8, Stat-Ease, Inc., MN, USA).

The effects of four independent variables (amount of multi-wall carbon nanotubes (MWCNTs), amount of TiF<sub>4</sub>, hydrothermal temperature and hydrothermal time) on the synthesis of MWCNTs–TiO<sub>2</sub> composite photocatalysts were investigated in detail using CCD with the form of RSM, and the photocatalytic degradation efficiency of gaseous styrene was selected as the response. The four chosen variables were converted to dimensionless ones (A, B, C, D), with the coded values at levels: −2, −1, 0, +1, +2. The determined values of the variables are presented in Table 1.

It should be mentioned that the values of the selected variables were determined according to our preliminary experiments. From the table, it can be seen that the five levels for controlling factors are 0.01, 0.03, 0.05, 0.07 and 0.09 g for the factor A, amount of MWCNTs; 0.02, 0.11, 0.20, 0.29 and 0.38 g for the factor B, amount of TiF<sub>4</sub>; 120, 150, 180, 210 and 240 °C for the factor C, hydrothermal temperature; and 12, 32, 52, 72 and 92 h for the factor D, hydrothermal time. Thus, a total of 28 experimental runs were performed in present study with four replications at the center point. The complete experimental design matrix and the responses are shown in Table 2.

### 2.2. Synthesis and characterization of photocatalysts

MWCNTs–TiO<sub>2</sub> composite photocatalysts were prepared using a facile one-step hydrothermal method. In a typical synthesis, MWCNTs (Shenzhen Nanotech Port Co., Ltd., China) was firstly purified by a mixture of concentrated sulfuric acid (95–98%) and nitric acid (65–68%) with a volume ratio of 3:1 under the temperature of 90 °C for 90 min. Then, a given amount of purified MWCNTs was dispersed in 40 mL of TiF<sub>4</sub> aqueous solution (Acros Organics, 99%) with different concentrations. After ultrasonic treatment for 30 min, the mixtures were transformed into Teflon-line autoclave with a volume of 100 mL and kept at selected hydrothermal temperature for different durations. After reaction, the products were collected by centrifuge, and then washed with distilled water thoroughly and finally dried at 80 °C for 8 h.

The synthesized composite photocatalysts were comprehensively characterized by X-ray diffractometer (XRD, Rigaku Dmax X-ray diffractometer), UV–visible spectrophotometer (UV–vis, UV-2501PC) and Scanning electron microscopy (SEM, Quanta 400F).

### 2.3. Photocatalytic degradation experiments

The photocatalytic activities of the prepared MWCNTs–TiO<sub>2</sub> composite photocatalysts were tested by the degradation of gaseous styrene with the initial concentration of 25 ± 1.5 ppmv operating in a continuous flow mode. In a typical reaction process, 0.1 g of the prepared composite photocatalyst was filled in a custom-made cubic quartz glass reactor with the size of 1.0 cm × 1.0 cm × 0.5 cm, top of which was a 365 nm UV-LED spot lamp (Shenzhen Lamplic Science Co., Ltd) fixed vertically with the distance of 6 cm. Dry air was used as a carrier gas and the total flow rate was 20 mL/min controlled by a flow meter. Before the lamp was switched on, the gaseous styrene was allowed to reach gas–solid adsorption equilibrium. The concentrations of gaseous styrene were analyzed by a gas chromatography (GC-900A) equipped with a flame ionization detector. The temperatures of the column, injector and detector were 110, 230 and 230 °C, respectively. Gas samples were collected at regular intervals using a gas-tight locking syringe (Agilent, Australia), and a 200 µL of gas sample was injected into the column for concentration determination in the splitless mode.

**Table 2**  
Experimental design matrix and the value of responses based on experiment run.

Run	Independent variables				Degradation efficiency (%)	
	A	B	C	D	Experimental	Predicted
1	0.03	0.11	210	32	40.9	40.6
2	0.01	0.20	180	52	46.8	49.3
3	0.05	0.20	120	52	60.5	62.3
4	0.07	0.29	210	72	30.1	31.9
5	0.05	0.02	180	52	35.1	37.4
6	0.07	0.11	210	32	32.3	33.2
7	0.05	0.20	180	52	48.3	48.3
8	0.07	0.29	150	32	40.3	40.7
9	0.03	0.29	210	72	34.1	33.6
10	0.07	0.11	210	72	38.3	37.0
11	0.07	0.11	150	32	38.2	38.1
12	0.05	0.20	240	52	39.2	38.1
13	0.03	0.29	150	72	53.9	52.9
14	0.03	0.29	210	32	33.3	33.1
15	0.07	0.11	150	72	46.2	46.3
16	0.07	0.29	150	72	45.4	45.1
17	0.05	0.20	180	12	38.9	38.0
18	0.07	0.29	210	32	30.4	31.9
19	0.03	0.11	150	32	53.4	51.5
20	0.05	0.20	180	52	48.2	48.3
21	0.03	0.11	150	72	62.3	60.2
22	0.05	0.20	180	52	48.6	48.3
23	0.03	0.29	150	32	47.2	48.0
24	0.05	0.20	180	52	48.1	48.3
25	0.05	0.20	180	92	45.1	46.7
26	0.05	0.38	180	52	30.3	28.7
27	0.03	0.11	210	72	45.3	44.8
28	0.09	0.20	180	52	35.9	34.1

### 3. Results and discussion

#### 3.1. Model establishment and analysis

Based on the experimental results listed in Table 2, a semi-empirical expression in Eq. (1) which is consisted of 15 statistically significant coefficients is obtained and expressed as follows:

$$Y = 48.30 - 3.79A - 2.16B - 6.03C + 2.17D + 1.54AB + 1.51AC - 0.13AD - 0.97BC - 0.94BD - 1.11CD - 1.65A^2 - 3.82B^2 + 0.47C^2 - 1.49D^2 \quad (1)$$

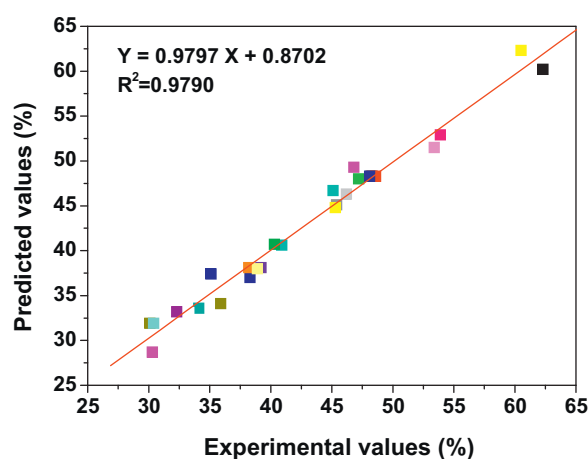
where  $Y$  is the response variable of degradation efficiency of styrene. The  $A$ ,  $B$ ,  $C$  and  $D$  represent four experimental factors, respectively.

The adequacy and significance of this model are discussed as follows. Eq. (1) is used to predict the photocatalytic degradation efficiencies of styrene by the prepared MWCNTs–TiO<sub>2</sub> composites with varied parameters within the selected range, and the experimental as well as predicted values are shown in Table 2. It is found that the predicted degradation efficiencies for styrene from the model match with the experimental values very well. This can be further evidenced by plotting the predicted photocatalytic values against the experimental values as shown in Fig. 1, where the line of the best fit with the slope of 0.9797 and  $R^2 = 0.9790$  were obtained. This demonstrates that the established model is very suitable to explain the experimental range studied. Moreover, adjusted  $R^2$  (0.9565, see Table 3) is very close to the corresponding  $R^2$  value, which further confirms the adaptability of this model [20].

In addition to correlation coefficient, the residuals (difference between the values of response from experiment and prediction) can be also applied to evaluate the adequacy of the model. The internally studentized residual plot is given in Fig. S1. It can be seen from Fig. S1a that all residuals are well distributed along the straight line, indicating that there is no severe non-normality. Moreover, Fig. S1b shows that the residuals are also distributed between  $-3$

and  $+3$  without any systematic structure and obvious pattern no matter how the predicted value varies. From these results, it can be concluded that the residuals appear to be a random scatter and the model obtained is adequate to describe the relationship between the degradation efficiency and the synthesis parameters for the preparation of MWCNTs–TiO<sub>2</sub> composites.

Table 3 displays the analysis of variance of the quadratic model, which is also required to test the significance and adequacy of the model [25,26]. If the model is adequacy,  $F$ -value (the ratio between the mean square of the model and the residual error) should be greater than the tabulated value of  $F$ -distribution for a certain number of degrees of freedom in the model at a level of significance [20]. From Table 3, it is found that the  $F$ -value for regression of the degradation model is 43.38, which is much greater than the value of  $F_{(14, 13)} (2.55)$  at 95% significance, indicating the adequacy of the model.



**Fig. 1.** Correlation between the predicted and experimental degradation efficiencies of styrene by MWCNTs–TiO<sub>2</sub> composite photocatalysts.

**Table 3**  
Analysis of variance for fit of degradation efficiency of styrene.

Source of variations	Sum of squares	Degree of freedom	Mean square	F-value
Regression	2006.24	14	143.30	43.38
Residuals	42.95	13	3.30	
Correction total	2049.19			

$R^2 = 0.9790$ , adjusted  $R^2 = 0.9565$ .

In order to find out the importance of the selected factors in Eq. (1), the Pareto analysis is also used and the percentage effect of each variable on the response can be calculated according to the following relation [27]:

$$P_i = \left( \frac{a_i^2}{\sum a_i^2} \right) \times 100 (i \neq 0) \quad (2)$$

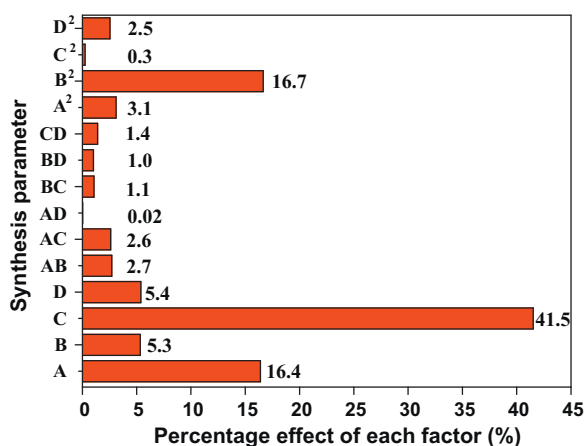
where  $P_i$  represents the percentage effect of each variable and  $a_i$  represents statistically significant coefficients in Eq. (1), respectively.

The corresponding results of the Pareto graphic analysis is shown in Fig. 2. As can be seen from the figure, the most important parameter for the preparation of MWCNTs–TiO<sub>2</sub> composite photocatalysts with high degradation efficiency for styrene is hydrothermal temperature (C, 41.5%), followed by the amount of MWCNTs (A, 16.4%), while hydrothermal time (D, 5.4%) and amount of TiF<sub>4</sub> (B, 5.3%) play less important roles in this work. Moreover, the degradation efficiency is also affected by the interrelated variables such as two factor interactions ( $B^2$ , 16.7%).

### 3.2. Analysis of contour and response surface plots

The two-dimensional contour and three-dimensional response surface plots are constructed by using the statistical software to illustrate the interaction effects of selected factors on the degradation efficiency and finally find out the optimal parameters for synthesis of MWCNTs–TiO<sub>2</sub> composite photocatalyst with the highest degradation efficiency of styrene. All plots are shown in Fig. 3. Moreover, in order to establish the relationship between the synthesis parameters and the degradation efficiency, the XRD patterns, UV–vis absorption spectra and SEM images of some typically prepared MWCNTs–TiO<sub>2</sub> composite photocatalysts are also displayed in Figs. 4–9.

Fig. 3a illustrates the effect of the amount of MWCNTs and hydrothermal temperature on the degradation efficiency of styrene (amount of TiF<sub>4</sub>, 0.20 g; hydrothermal time of 52 h). As can be seen that, when the amount of MWCNTs increases from 0.01 to

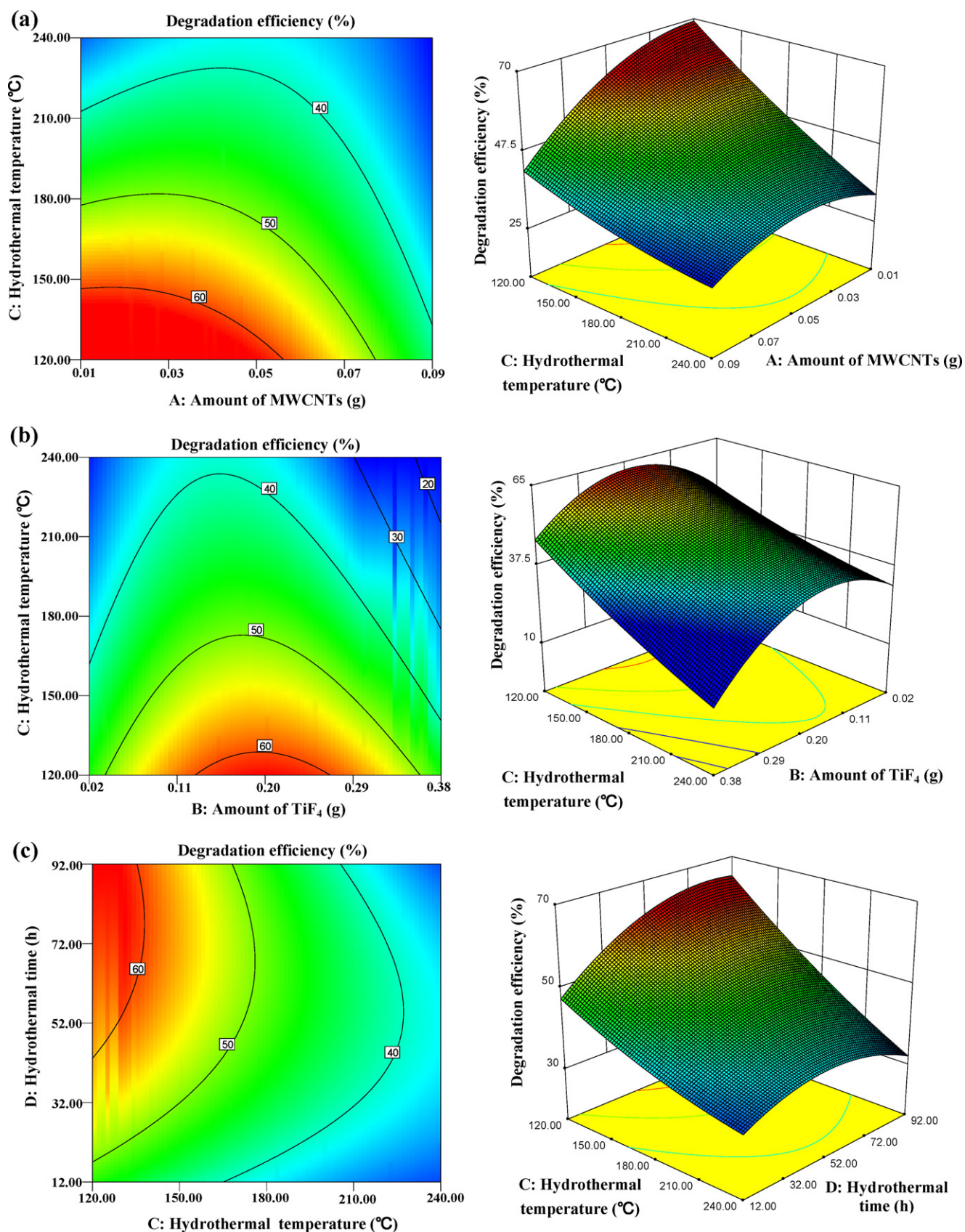


**Fig. 2.** Pareto graphic analysis for the degradation efficiency of styrene by MWCNTs–TiO<sub>2</sub> composite photocatalysts.

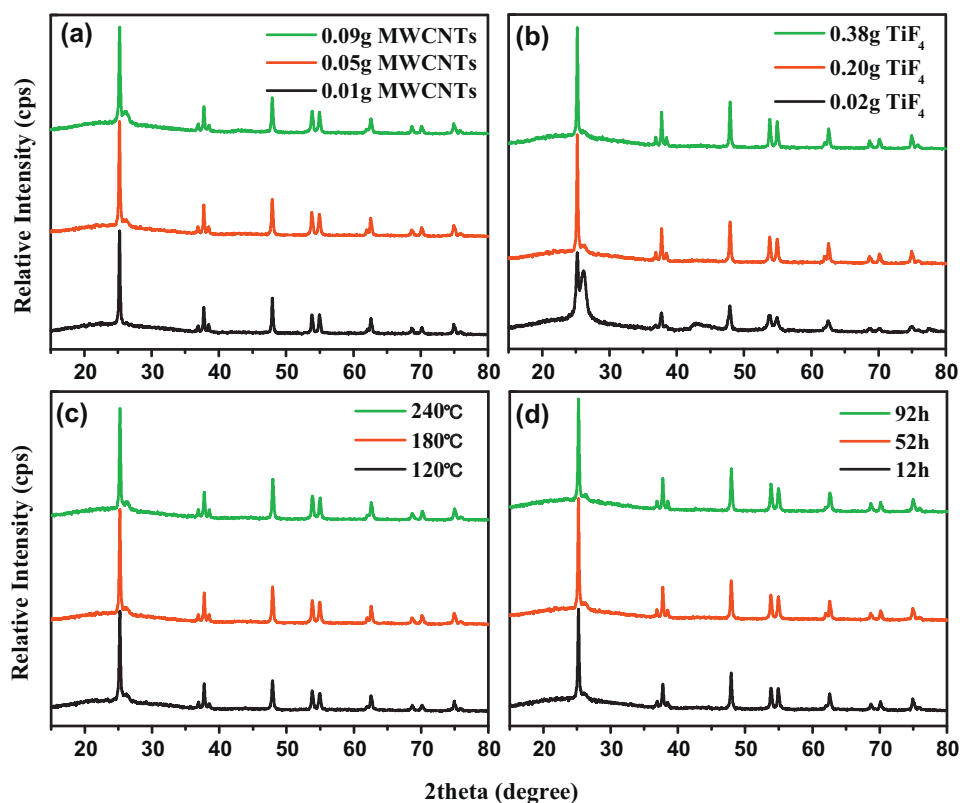
0.05 g, the degradation efficiency slightly increases from 46.8 to 48.3% and peaks at 48.3%. However, with further increase of the amount of MWCNTs to 0.09 g, the degradation efficiency decreases significantly to 35.9%. Proper explanation can be obtained from the characteristic results shown in Figs. 4a, 5a and 6. When 0.01 g MWCNTs is added into the composite photocatalyst, the resulted composite photocatalyst is consisted of MWCNTs (unable to be detected by XRD due to the low content) and anatase TiO<sub>2</sub> spheres with the average diameter of about 800 nm. Further observation indicates that the TiO<sub>2</sub> spheres are covered by well-defined exposed crystal facets (see insert of Fig. 6a), which are convenient for the light reflecting/scattering and lead to high light harvesting efficiency [28]. With increasing the content of MWCNTs to 0.05 g, besides the characteristic peaks of anatase TiO<sub>2</sub>, a small peak at  $2\theta = 26.0^\circ$  for MWCNTs can be observed from the XRD pattern (see Fig. 4a), and the average diameter of TiO<sub>2</sub> spheres is maintained at about 800 nm while the well-defined exposed {001} crystal facets on the TiO<sub>2</sub> spheres are hardly discerned (see Fig. 6b). Moreover, the UV absorption intensity slightly decreases (see Fig. 5a), which may be due to the disappearance of the well-defined exposed {001} crystal facets and the increase of amount of MWCNTs preventing TiO<sub>2</sub> from light absorption. On the other hand, the increase of the amount of MWCNTs can also enhance the adsorption and enrichment capacity of the composite photocatalyst to organics [29]. As known, the adsorption of pollutants onto the photocatalyst surface is the first step of photocatalytic reaction, and the higher the adsorption capacity was, the greater the photocatalytic reaction rate constant was [8]. Herein, the increase of the photocatalytic degradation efficiency for styrene is positive correlated with the amount of MWCNTs (within the range of 0.01–0.05 g), which may be attributed to higher increase of the synergetic effect (due to the increase of the adsorption capacity) than the decrease of the UV absorption ability. However, with further increasing the content of MWCNTs to 0.09 g, MWCNTs can be easily detected in the prepared composite photocatalyst by XRD (the diffraction peak at  $2\theta = 26.0^\circ$  for MWCNTs). Moreover, few TiO<sub>2</sub> particles can be observed which are covered by the excess MWCNTs (see Fig. 6c), leading to the further decrease of the absorption intensity in the UV region due to the shielding of the UV light for the absorption by TiO<sub>2</sub> with excess MWCNTs, and thus resulting in the decrease of the degradation efficiency.

In the case of hydrothermal temperature, it is found from Fig. 3a that the degradation efficiency continuously decreases from 60.5 to 39.2% with the increase of the hydrothermal temperature from 120 to 240 °C. This result may be attributed to the different structural, optical and morphological properties of the composite photocatalysts as displayed in Figs. 4c, 5c and 7. From Fig. 4c, it can be seen that all composite photocatalysts show the similar XRD patterns no matter how the hydrothermal temperature changes, indicating that low hydrothermal temperature such as 120 °C is enough for the formation of the MWCNTs–anatase TiO<sub>2</sub> composite photocatalysts. However, the average diameter of the TiO<sub>2</sub> particles in the composite photocatalyst sharply increases from about 400 to 800 nm with increasing the hydrothermal temperature from 120 (see Fig. 7a) to 180 °C (see Fig. 7b), and continuously increases to about 1 μm when the hydrothermal temperature further increases to 240 °C (see Fig. 7c). On the contrary, the continuous decrease

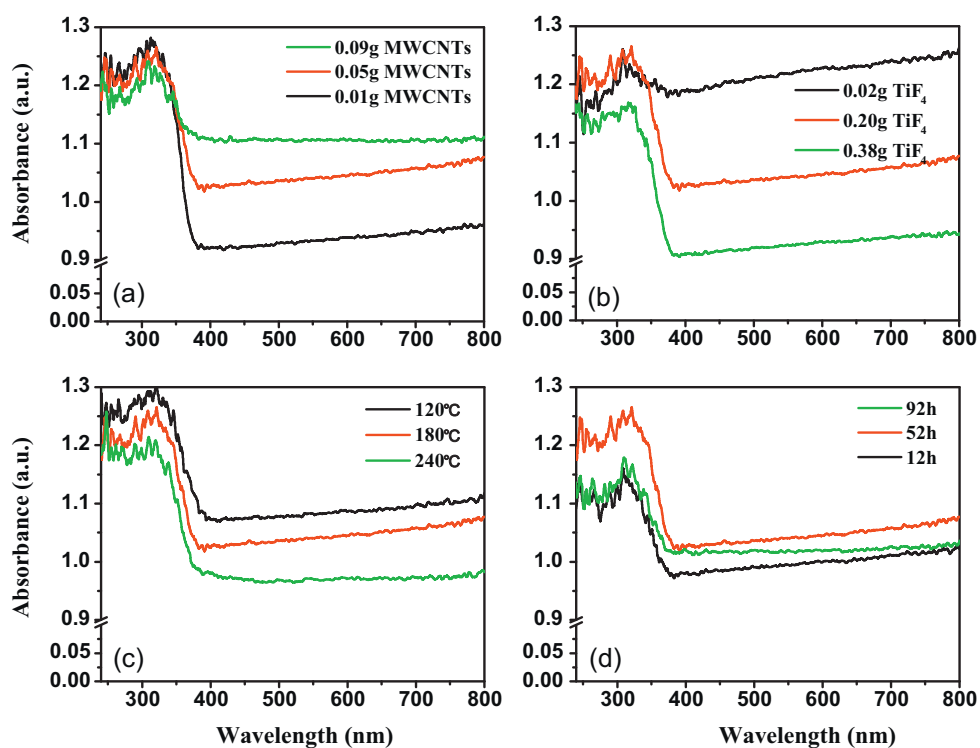




**Fig. 3.** The contour and response surface plots of degradation efficiency of styrene by MWCNTs– $\text{TiO}_2$  composite photocatalysts as the function of (a) amount of MWCNTs with hydrothermal temperature, (b) amount of  $\text{TiF}_4$  with hydrothermal temperature, and (c) hydrothermal temperature with hydrothermal time.

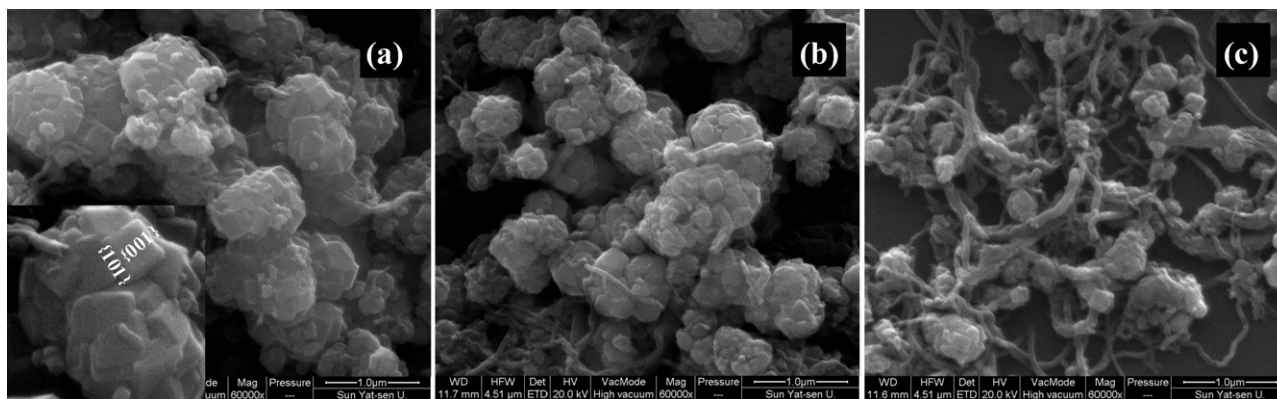


**Fig. 4.** XRD patterns of composite photocatalysts prepared with different (a) amount of MWCNTs (the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal temperature, 180 °C; hydrothermal treatment for 52 h); (b) amount of  $\text{TiF}_4$  (the amount of MWCNTs, 0.05 g; hydrothermal temperature, 180 °C; hydrothermal treatment for 52 h); (c) hydrothermal temperature (the amount of MWCNTs, 0.05 g; the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal treatment for 52 h); (d) hydrothermal time (the amount of MWCNTs, 0.05 g; the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal temperature, 180 °C).

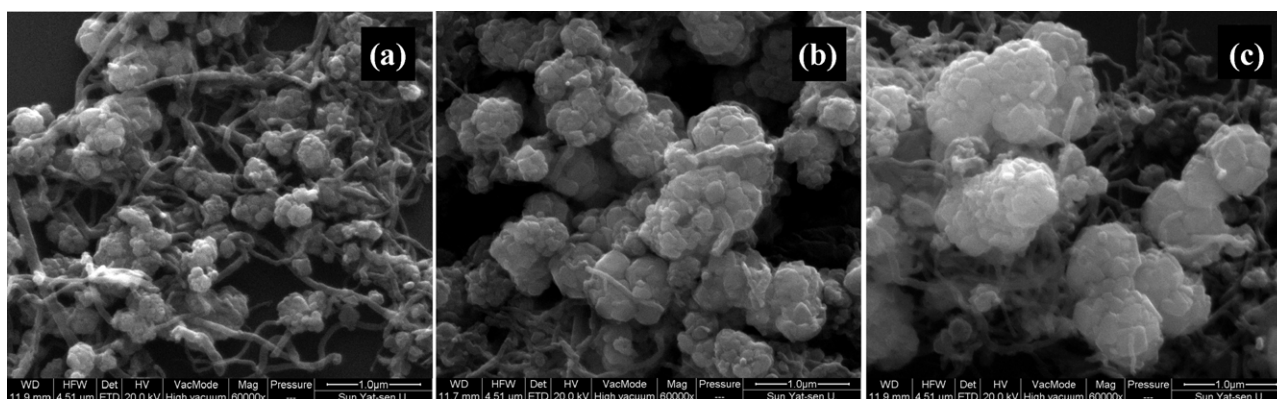


**Fig. 5.** UV-vis absorption spectra of composite photocatalysts prepared with different (a) amount of MWCNTs (the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal temperature, 180 °C; hydrothermal treatment for 52 h); (b) amount of  $\text{TiF}_4$  (the amount of MWCNTs, 0.05 g; hydrothermal temperature, 180 °C; hydrothermal treatment for 52 h); (c) hydrothermal temperature (the amount of MWCNTs, 0.05 g; the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal treatment for 52 h); (d) hydrothermal time (the amount of MWCNTs, 0.05 g; the amount of  $\text{TiF}_4$ , 0.20 g; hydrothermal temperature, 180 °C).





**Fig. 6.** SEM images of composite photocatalysts prepared with 0.20 g  $\text{TiF}_4$ , hydrothermal temperature of  $180^\circ\text{C}$ , hydrothermal time of 52 h, and (a): 0.01 g; (b): 0.05 g; (c): 0.09 g MWCNTs.

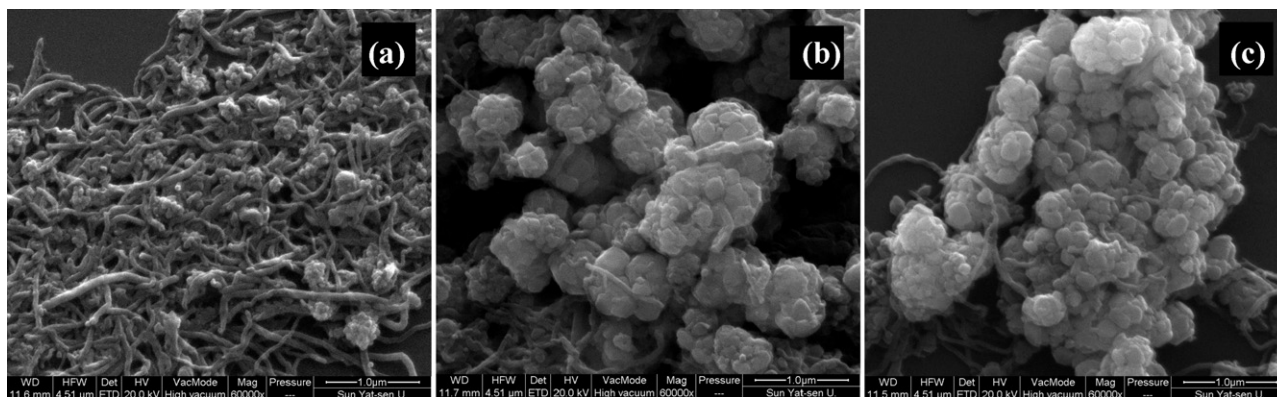


**Fig. 7.** SEM images of composite photocatalysts prepared with 0.05 g MWCNTs, 0.20 g  $\text{TiF}_4$ , hydrothermal time of 52 h and hydrothermal temperature of (a):  $120^\circ\text{C}$ ; (b):  $180^\circ\text{C}$ ; (c):  $240^\circ\text{C}$ .

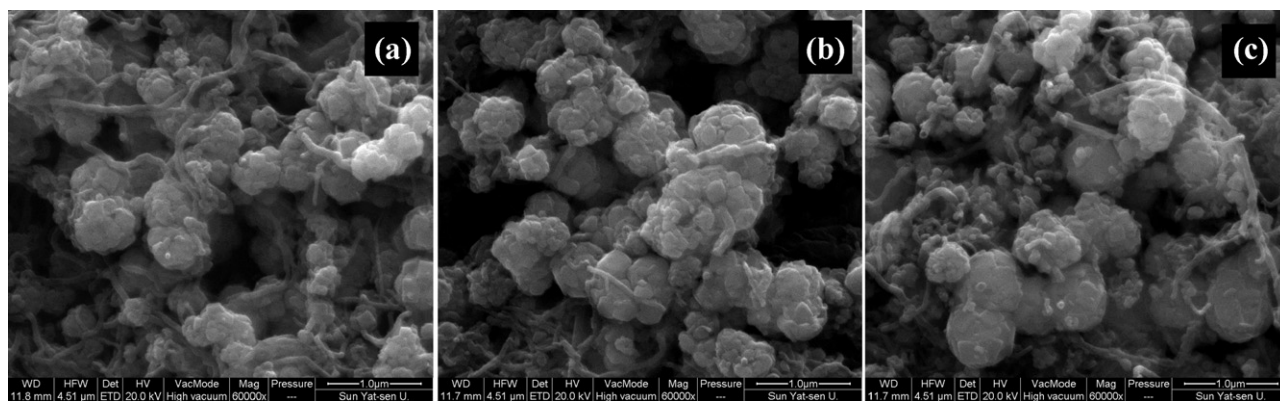
of UV absorption intensity is observed with the increase of the hydrothermal temperature from  $120$  to  $240^\circ\text{C}$  (see Fig. 5c). All above-mentioned results indicate that the MWCNTs– $\text{TiO}_2$  composite photocatalyst with smallest  $\text{TiO}_2$  spheres and highest UV absorption ability, which possesses the best photocatalytic activity towards degradation of styrene, was synthesized under lowest hydrothermal temperature. This is because that the large specific area of small-sized  $\text{TiO}_2$  particles ensures efficient UV light absorption and provides more photoreactive sites for degradation reactions [17]. Furthermore, it was found that lower hydrothermal temperature was in favor of synthesizing composite photocatalyst with larger specific surface area, leading to higher photocatalytic

performance [30]. Therefore, the highest degradation efficiency is obtained for the MWCNTs– $\text{TiO}_2$  composite prepared with a suitable amount of MWCNTs addition and minimum hydrothermal temperature ( $120^\circ\text{C}$ ).

Fig. 3b shows the effect of amount of  $\text{TiF}_4$  and hydrothermal temperature on the photocatalytic degradation efficiency of styrene (amount of MWCNTs, 0.05 g; hydrothermal time, 52 h). Similar to the result obtained above, the highest degradation efficiency is achieved when the hydrothermal temperature is maintained at its minimum ( $120^\circ\text{C}$ ). In the case of amount of  $\text{TiF}_4$ , there is a notable increase in degradation efficiency from 35.1 to 48.3% with increasing the amount of  $\text{TiF}_4$  from 0.02 to 0.20 g. However, further



**Fig. 8.** SEM images of composite photocatalysts prepared with 0.05 g MWCNTs, hydrothermal temperature of  $180^\circ\text{C}$ , hydrothermal time of 52 h, and (a): 0.02 g; (b): 0.20 g; (c): 0.38 g  $\text{TiF}_4$ .



**Fig. 9.** SEM images of composite photocatalysts prepared with 0.05 g MWCNTs, 0.20 g  $\text{TiF}_4$ , hydrothermal temperature of 180 °C and hydrothermal time of (a): 12 h; (b): 52 h; (c): 92 h.

increase of the amount of  $\text{TiF}_4$  to 0.38 g can lead to the decrease of the degradation efficiency to 30.3%. From the results of XRD patterns (Fig. 4b) and SEM images (Fig. 8) of the MWCNTs– $\text{TiO}_2$  composite photocatalysts, it is clear to see that the intensity of diffraction peak at  $2\theta = 26.0^\circ$  for MWCNTs is rapidly weakened and more  $\text{TiO}_2$  particles can be observed in the composites with the increase of the amount addition of  $\text{TiF}_4$  from 0.02 to 0.20 g (see Fig. 8a and b), leading to the increase of the absorption intensity in the UV region (see Fig. 5b), which is attributed to the electron transition of  $\text{TiO}_2$  from the valence band to conduction band [31]. However, with further increasing the amount addition of  $\text{TiF}_4$  to 0.38 g, the  $\text{TiO}_2$  particles in the composite agglomerate to form large particles with size of about several micrometers (see Fig. 8c) and the UV absorption intensity decreases rapidly (see Fig. 5b) due to the decrease of specific surface area. All these confirm that the composite photocatalyst prepared with lower or higher amount addition of  $\text{TiF}_4$  possesses worse photocatalytic activity in this work.

To investigate the effect of hydrothermal temperature and hydrothermal time on the photocatalytic degradation efficiency of gaseous styrene, the degradation experiments are conducted using MWCNTs– $\text{TiO}_2$  composite photocatalysts prepared with different hydrothermal temperature and time varying from 120 to 240 °C and 12 to 92 h, respectively, at constant amount of MWCNTs (0.05 g) and  $\text{TiF}_4$  (0.20 g). The results shown in Fig. 3c again indicate that the highest degradation efficiency is obtained when the hydrothermal temperature is kept at its minimum. Moreover, it is found that, with the increase of the hydrothermal time from 12 to 52 and then to 92 h, the degradation efficiency firstly increases steadily from 38.9 to 48.3% and then slightly decrease to 45.1%. The XRD patterns and SEM images shown in Figs. 4d and 9 demonstrate that hydrothermal time has a negligible effect on the structure and morphology of the composite photocatalysts, and the short hydrothermal time of 12 h is enough to form the composite photocatalysts composed of  $\text{TiO}_2$  spheres with the average diameter of about 800 nm together with MWCNTs. In addition, it can be seen from Fig. 5d that the absorption intensity in the UV region increases firstly with the increase of hydrothermal time from 12 to 52 h, which may be due to the increased synergistic interaction (for example, the chemical bonding) between  $\text{TiO}_2$  particles and MWCNTs [6]. And then the UV absorption intensity decreases when the hydrothermal time is extended to 92 h, though it is even stronger than that of composite photocatalyst prepared with the hydrothermal time of 12 h, implying the synergistic interaction is slightly weakened. This result suggests that UV absorption ability plays a key role during the photocatalytic degradation reaction for the composite photocatalysts prepared with different hydrothermal time, and too short or too long hydrothermal time is not beneficial for synthesizing the

composite photocatalyst with higher UV absorption intensity and then higher photocatalytic activity.

To further prove the significant role of the UV absorption ability in the photocatalytic reaction, the XRD patterns, SEM images and UV–vis absorption spectra of MWCNTs– $\text{TiO}_2$  composite photocatalysts with the highest (62.3%, named as composite A) and lowest (30.1%, named as composite B) degradation efficiencies for styrene are compared and shown in Figs. S2–S4 (Supporting Information). Similar XRD patterns are observed for composite A and B (see Fig. S2). However, obvious difference can be discerned from the SEM images (see Fig. S3) and UV–vis absorption spectra (see Fig. S4). From Fig. S3, it can be seen that, although the composites A and B are all consist of MWCNTs and  $\text{TiO}_2$  spheres, the average diameters of  $\text{TiO}_2$  spheres are about 200 and 800 nm, respectively. Apparently, the  $\text{TiO}_2$  particles in composite A is much smaller than that in composite B, which results in a stronger UV absorption for composite A (see Fig. S4). To sum up, in the present study, the stronger UV absorption of the MWCNTs– $\text{TiO}_2$  composite photocatalyst controlled by the synthesis parameters is, the higher of the degradation efficiency is obtained for styrene.

Overall, the main objective of the optimization in this study is to effectively obtain the optimum synthesis parameters for the preparation of MWCNTs– $\text{TiO}_2$  composite photocatalyst with highest photocatalytic degradation efficiency of gaseous styrene based on the experimental results. Herein, by using a numerical optimization method in the Design Expert software, the desired goals for all the variables are chosen in the experimental range that the amount of MWCNTs, the amount of  $\text{TiF}_4$ , hydrothermal temperature and hydrothermal time are in the range of 0.01–0.09 g, 0.02–0.38 g, 120–240 °C and 12–92 h, respectively, while the degradation efficiency is defined as “maximize” with the upper limit of 100% (the theoretical high). Then, the optimum values of the variables for synthesis of MWCNTs– $\text{TiO}_2$  composite photocatalyst with the highest degradation efficiency (74.4%) for styrene are 0.01 g, 0.14 g, 120 °C and 87.2 h for amount of MWCNTs, amount of  $\text{TiF}_4$ , hydrothermal temperature and hydrothermal time, respectively.

#### 4. Conclusions

In this study, the RSM was firstly applied in the optimizing the synthesis of MWCNTs– $\text{TiO}_2$  composite photocatalyst with the highest photocatalytic degradation efficiency of gaseous styrene. Among the synthesis parameters in the experimental design, the hydrothermal temperature played the most important role to influence the photocatalytic degradation activity of MWCNTs– $\text{TiO}_2$  for gaseous styrene. Lower hydrothermal temperature was beneficial for synthesizing the MWCNTs– $\text{TiO}_2$  composite with higher degradation efficiency for styrene. Meanwhile, other three



synthesis parameters, such as amount of MWCNTs, hydrothermal time and amount of  $\text{TiF}_4$  also showed the influence to the degradation efficiency of the composite photocatalysts. Worse photocatalytic degradation efficiency for styrene was obtained when the composite photocatalysts were prepared under these parameters with lower or higher values. By combining the degradation results and physical properties of the prepared composite photocatalysts, it was found that the absorption ability in the UV region determined the photocatalytic activity of the MWCNTs– $\text{TiO}_2$  composite photocatalyst for gaseous styrene. The stronger UV absorption the MWCNTs– $\text{TiO}_2$  composite photocatalyst is, the higher the degradation efficiency for styrene can be obtained. Finally, the optimum values of synthesis parameters were obtained based on the experimental data which were 0.01 g, 0.14 g,  $120^\circ\text{C}$  and 87.2 h for the amount of MWCNTs, the amount of  $\text{TiF}_4$ , hydrothermal temperature and hydrothermal time, respectively.

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### Appendix A. Supplementary data

Supplementary data associated with this article can be found, in the online version, at <http://dx.doi.org/10.1016/j.apcatb.2012.04.020>.

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